

Facile Preparation of Fluoroalkyl End-Capped Vinyltrimethoxysilane Oligomer/Sand Composites Possessing Superoleophilic/Superhydrophobic Characteristic: Application to Oil/Water Separation and Selective Removal of Fluorinated Aromatic Compounds from Aqueous Methanol Solution

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How to cite this paper: Sawada, H., Tono, K. and Yamashita, K. (2022) Facile Preparation of Fluoroalkyl End-Capped Vinyltrimethoxysilane Oligomer/Sand Composites Possessing Superoleophilic/Superhydrophobic Characteristic: Application to Oil/Water Separation and Selective Removal of Fluorinated Aromatic Compounds from Aqueous Methanol Solution. *Open Journal of Composite Materials*, 12, 56-71.

<https://doi.org/10.4236/ojcm.2022.121005>

Received: December 15, 2021

Accepted: January 27, 2022

Published: January 30, 2022

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Abstract

Fluoroalkyl end-capped vinyltrimethoxysilane oligomer

$[R_F-(CH_2-CHSi(OMe)_3)_n-R_F]$: $n = 2, 3$, $R_F = CF(CF_3)OC_3F_7$: $R_F-(VM)_n-R_F$, was applied to the facile preparation of the corresponding oligomer/sand (Ottawa sand: OS) composites $[R_F-(VM-SiO_{3/2})_n-R_F/OS]$ through the sol-gel reaction of the oligomer in the presence of micro-sized OS particles (590 - 840 μm) under alkaline conditions at room temperature. FE-SEM (Field Emission Scanning Electron Micrograph) images showed that the obtained composites consist of the $R_F-(VM-SiO_{3/2})_n-R_F$ oligomeric nanoparticles and the micro-sized OS particles. Interestingly, the $R_F-(VM-SiO_{3/2})_n-R_F/OS$ composites thus obtained can provide the superoleophilic/superhydrophobic characteristic on the composite surface, applying to the separation of not only the mixture of oil/water but also the W/O emulsion to isolate the transparent colorless oil. The fluorinated oligomeric OS composites were also found to be applicable to the selective removal of fluorinated aromatic compounds from an aqueous methanol solution. Especially, it was demonstrated that the fluorinated OS composites can supply a higher efficient and smooth separation ability for the separation of the mixture of oil and water than that of the corresponding fluori-

nated micro-sized controlled silica gel (μ -SiO₂) composites (average particle size: 9.5 μ m), which were prepared under similar conditions. In addition to the separation of oil/water, the fluorinated OS composites provided higher and more selective removal ability for the fluorinated aromatic compounds from aqueous solutions than that of the μ -SiO₂ composites.

Keywords

Fluorinated Oligomeric Composite, Micro-Sized Ottawa Sand Particle, Superoleophilic/Superhydrophobic Property, Smooth Separation of Oil and Water, Selective Removal of Fluorinated Aromatic Compound

1. Introduction

Due to the serious problems related to oil spill accidents in the environment induced by the disasters in living systems and a growing body of occurrence of industrial oily wastewater, oil/water separation has been the subject of practical research of the world [1] [2] [3] [4]. In fact, there has been a large volume of reports on the development of the functional materials with superhydrophobic/superoleophilic surfaces to separate the mixture of oil and water [5] [6] [7] [8]. From the practical point of view, it is of particular importance to fabricate the low-cost materials possessing higher efficiency and fast separation ability of oil/water. It is well-known that micro-sized silica gel particles can supply a wide range of practical use such as adsorbents and the packing material for column chromatography. Thus, the practical application of micro-size silica gels to the superhydrophobic/superoleophilic composites is of great significance owing to the development of novel materials for the separation of oil and water, because silica gels are in general low-cost popular materials. In fact, we have recently reported on the preparation of the fluoroalkyl end-capped oligomeric micro-sized silica gel composite particles possessing superoleophilic/superhydrophobic characteristic to separate the mixture of oil and water [9].

In addition to the serious problems in increasing environmental pollution related to the oil spill into the ocean as indicated above, a large volume of fluorinated drugs and pesticides have recently come to the market, and made up about 20% of the pharmaceuticals and over 30% of all agrochemicals, respectively [10]-[15]. Therefore, it is deeply desirable to develop the practical removal technologies of not only the oils but also the fluorinated organic micropollutants including their raw materials and intermediates from industrial wastewater. The main component of sand is silicon dioxide, quite similar to that of the silica gel, and sand is also an abundant natural resource. Therefore, the sand should become a good candidate for novel composite materials for the practical removal of oil from wastewater, due to its low cost and nontoxicity to the environment, excellent chemical and physical stability. In fact, attractive attention has been recently focused on the sand composites possessing superhydrophobic characteristic, which can be

fabricated by the reactions of 1, 1, 1, 3, 3, 3-hexamethyldisilazane [16], 1*H*, 1*H*, 2*H*, 2*H*-perfluorodecyltrichlorosilane [17], 1*H*, 1*H*, 2*H*, 2*H*-perfluorooctyltriethoxysilane [18], octadecyltrichlorosilane [19] [20], and hexadecyltrimethoxysilane [21] [22] with the corresponding sands.

During a growing body of our studies on the two fluoroalkyl end-capped oligomers $[R_F-(M)_n-R_F]$; R_F = fluoroalkyl group; M: radical polymerizable monomers [23] [24] [25], we have already reported that two fluoroalkyl end-capped vinyltrimethoxysilane oligomer $[R_F-(CH_2CHSi(OMe)_3)_n-R_F]$, $n = 2, 3$; $R_F-(VM)_n-R_F]$ can form the nanometer-sized controlled self-assembled molecular aggregates in organic media such as methanol through the aggregation of terminal fluoroalkyl groups [26]. These fluorinated aggregates interact with a variety of guest molecules [**Guest**] such as gold nanoparticles, hydroxyapatite, zinc oxide and titanium oxide to provide the corresponding fluorinated oligomeric silica/**Guest** nanocomposites $[R_F-(CH_2CHSiO_{3/2})_n-R_F/**Guest**]$ possessing not only a surface-active property imparted by fluorine but also a unique characteristic related to each **Guest** molecule [26]. Therefore, it is of practical interest to prepare the sand composites by the use of the $R_F-(VM)_n-R_F$ oligomer as a key intermediate. Herein we report on the preparation of fluoroalkyl end-capped vinyltrimethoxysilane oligomer/sand composites $[R_F-(CH_2CHSiO_{3/2})_n-R_F/sand]$ by the sol-gel reaction of the corresponding oligomer $[R_F-(VM)_n-R_F]$ in the presence of sand particles under alkaline conditions. In addition, we would like to demonstrate on the application of the $R_F-(CH_2CHSiO_{3/2})_n-R_F/sand$ composites to the separation of oil and water including the selective removal of fluorinated aromatic compounds from an aqueous methanol solution. These findings will be described in this article.

2. Experimental

2.1. Measurements

Micrometer size-controlled silica gel composite particles were analyzed by using laser diffraction particle size analyzer: Shimadzu SALD-200 V (Kyoto, Japan). Molecular weight of $R_F-(VM)_n-R_F$ oligomer was measured by using a Shodex DS-4 (pump, Tokyo, Japan) and Shodex RI-71 (detector) gel permeation chromatography calibrated with polystyrene standard using tetrahydrofuran as the eluent. Thermal analyses were recorded by raising the temperature around 800°C (the heating rate: 10°C/min) under atmospheric conditions by the use of Bruker axs TG-DTA2000SA differential thermobalance (Kanagawa, Japan). The contact angles were measured by the use of Kyowa Interface Science Drop Master 300 (Saitama, Japan). Ultraviolet-visible (UV-vis) spectra were measured using Shimadzu UV-1600 UV-vis spectrophotometer (Kyoto, Japan). Field emission scanning electron micrograph (FE-SEM) was recorded by using JEOL JSM-7000F (Tokyo, Japan). Energy dispersive X-ray (EDX) spectra were obtained using JEOL JSM-7000F (Tokyo, Japan). Aluminum crucible (40 mL; Material No: 27311) was purchased from Mettler-Toledo Co., Ltd. (Tokyo, Japan). Ultrasonic irradiation was used by As One Ultrasonic Cleaner US-3R (Tokyo, Japan). Optical and flu-

orescence microscopies were measured by using OLYMPUS Corporation BX51 (Tokyo, Japan).

2.2. Materials

Vinyltrimethoxysilane was used as received from Dow Corning Toray Co., Ltd. (Tokyo, Japan). Sand (Ottawa sand: OS, average particle size: 590 - 840 μm) was received from Restek Corporation (PA, USA). Micro-sized silica particles (Wako-gel^{TR} C-500HG: average particle size: 14 μm) and Acid Blue 112 were supplied from FUJIFILM Wako Pure Chemical Industries (Osaka, Japan) and Chugaikasei Co., Ltd. (Fukushima, Japan), respectively. Dodecane, 1,2-dichloroethane, Span 80, 4, 4'-bisphenol, octafluoro-4, 4'-biphenol, acetophenone, 2', 3', 4', 5', 6'-pentafluoroacetophenone, and trans-cinnamic acid were all received from Tokyo Chemical Industry Co., Ltd. (Tokyo, Japan). Trans-2,3,4,5,6-pentafluorocinnamic acid was purchased from Synquest Laboratories (FL, USA). Fluoroalkyl end-capped vinyltrimethoxysilane oligomer $[\text{R}_F\text{-(CH}_2\text{-CHSi(OMe)}_3)_n\text{-R}_F]$: the mixture of dimer and trimer; $\text{R}_F = \text{CF}(\text{CF}_3)\text{OC}_3\text{F}_7$ ($\text{R}_F\text{-(VM)}_n\text{-R}_F$); $\text{Mn} = 780$] was synthesized by reaction of fluoroalkanoyl peroxide with the corresponding monomer according to our previously reported method [27]. Solid-phase extraction cartridge connected with the polyethylene frit [Type Mini (0.1 mL)] was supplied by Tomoe-Works Co., Ltd. (Amagasaki, Japan).

2.3. Preparation of Fluoroalkyl End-Capped Vinyltrimethoxysilane Oligomer/Ottawa Sand (OS) Composites $[\text{R}_F\text{-(VM-SiO}_{3/2})_n\text{-R}_F/\text{OS}]$

A typical procedure for the facile preparation of $\text{R}_F\text{-(VM-SiO}_{3/2})_n\text{-R}_F/\text{OS}$ composites is as follows: To methanol solution (5 mL) containing fluoroalkyl end-capped vinyltrimethoxysilane oligomer $[\text{R}_F\text{-(VM)}_n\text{-R}_F]$ (50 mg) was added OS particles (150 mg). The mixture was stirred with a magnetic stirring bar at room temperature for 10 min. 25% aqueous ammonia solution (2.0 mL) was added to the methanol solution, and was successively stirred at room temperature for 5 hrs. After the solvent was evaporated off, the obtained product was dried under vacuum at 50°C for 1 day to produce the expected fluorinated composite white colored powders (166 mg). Other composites were prepared under similar conditions. The results are demonstrated in **Scheme 1** and **Table 1**. $\text{R}_F\text{-(VM-SiO}_{3/2})_n\text{-R}_F/\mu\text{-SiO}_2$ composites were also prepared by using micro-sized silica particles ($\mu\text{-SiO}_2$: average particle size: 14 μm) under similar conditions, for comparison (see **Scheme 2**).

2.4. Contact Angle Measurements of Dodecane and Water on the $\text{R}_F\text{-(VM-SiO}_{3/2})_n\text{-R}_F/\text{OS}$ composite Powders Surface

The $\text{R}_F\text{-(VM-SiO}_{3/2})_n\text{-R}_F/\text{OS}$ composite powders (2 mg) were added into the aluminum crucible (volume: 40 μL). The contact angles of dodecane and water were measured by the deposit of each droplet (2 μL) on the composite powders surface

at room temperature. The contact angle measurements of dodecane and water on the other composite powders were conducted under the similar conditions.

2.5. Preparation of the Surfactant-Stabilized Water-in-Oil (1,2-Dichloroethane) Emulsion

The surfactant (span 80:30 mg) was added into the mixture of water (0.05 mL) and 1,2-dichloroethane (5.0 mL). The expected white-colored W/O emulsion was easily prepared through the ultrasonic irradiation of the obtained mixture for 5 min at room temperature.

2.6. Removal of 2', 3', 4', 5', 6'-Pentafluoroacetophenone (PFAP) in Aqueous Methanol Solution by Using the $R_F-(CH_2CHSiO_{3/2})_n-R_F/OS$ Composite Powders

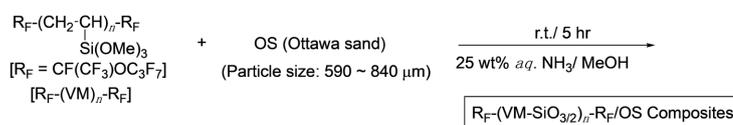
Solid-phase extraction cartridge connected with the polyethylene frit packed with the $R_F-(CH_2CHSiO_{3/2})_n-R_F/OS$ composite powders (10 mg; Run 1 in **Table 1**) was used for the removal of PFAP. 5 mL of aqueous methanol solution [$H_2O/MeOH$: 94/6 (vol/vol)] containing PFAP (30 mg/dm³) was applied to the cartridge, and the obtained eluent was analyzed by UV-vis spectra measurements to detect the residual PFAP. The residual amounts of other organic compounds were also analyzed under similar conditions. The results are summarized following.

3. Results and Discussion

Fluoroalkyl end-capped vinyltrimethoxysilane oligomer [$R_F-(VM)_n-R_F$] was found to undergo the sol-gel reaction in the presence of Ottawa sand (OS) particles under alkaline conditions at room temperature, providing the corresponding fluorinated oligomeric silica/OS composites. The results are depicted in **Scheme 1** and **Table 1**.

Scheme 1 and **Table 1** show that the expected composites can be easily obtained through the sol-gel reaction under alkaline conditions in good isolated yields: 64% - 97%. The content of each oligomer in the composites in **Table 1** was determined by using the thermogravimetric analyses (TGA), in which the weight loss of the composites was measured by raising the temperature around 800 °C at a 10 °C/min heating rate under air atmospheric conditions, and the results are also demonstrated in **Table 1**. TGA curves of some composites in **Table 1** are illustrated in **Figure 1**. The pristine OS powders and the $R_F-(VM-SiO_{3/2})_n-R_F$ oligomeric nanoparticles [28], which were prepared by the sol-gel reaction of the corresponding oligomer under alkaline conditions, are also shown in **Figure 1**, for comparison.

As shown in **Table 1** and **Figure 1**, the contents of oligomers were estimated



Scheme 1. Preparation of $R_F-(VM-SiO_{3/2})_n-R_F/OS$ composites.

Table 1. Preparation of $R_F-(VM-SiO_{3/2})_n-R_F/OS$ composites.

Run	$R_F-(VM)_n-R_F$ (mg)	OS (mg)	Yield (%)*	Content of oligomer in the composites (%)**
1	50	10	64	66
2	50	50	82	39
3	50	75	84	44
4	50	100	89	39
5	50	150	83	12
6	50	200	93	26
7	50	250	94	24
8	50	300	93	9
9	50	400	95	15
10	50	500	95	5
11	50	600	97	18
12	50	700	97	7

*Yield was based on oligomer and OS; **Content of oligomer in each composite was determined by using the weight loss value at 800°C of the composites and the $R_F-(VM-SiO_{3/2})_n-R_F$ oligomeric nanoparticles

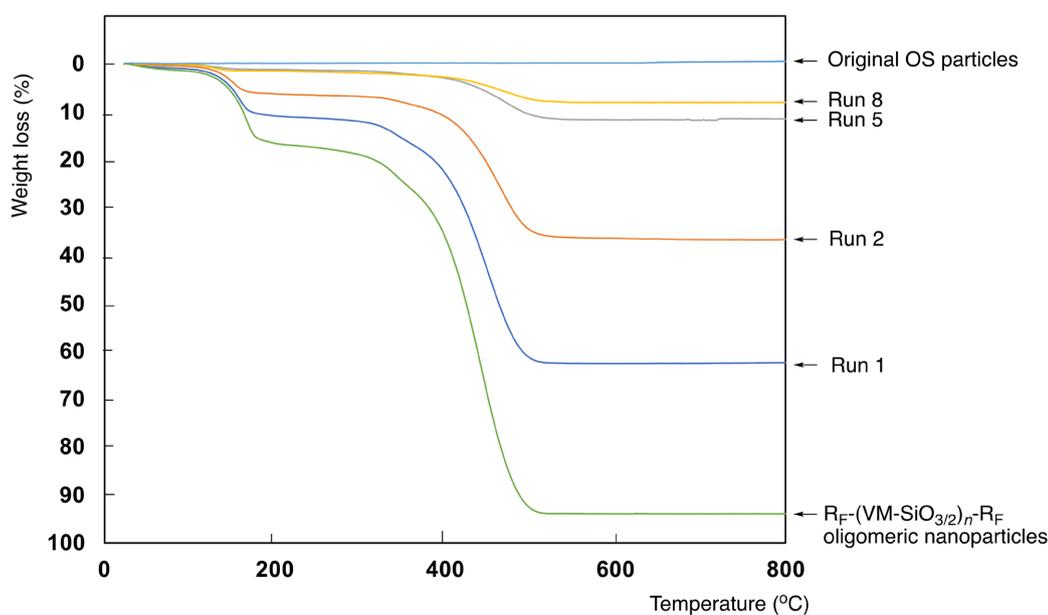


Figure 1. Thermogravimetric analysis (TGA) of the $R_F-(VM-SiO_{3/2})_n-R_F/OS$ composites (Runs 1, 2, 5 and 8 in **Table 1**), original OS particles, and $R_F-(VM-SiO_{3/2})_n-R_F$ oligomeric nanoparticles, which were prepared under the similar sol-gel reaction of the corresponding oligomer to that of **Scheme 1**.

to be 5% - 66% by the use of the TGA measurements. The contents of oligomers in the composites were found to decrease from 66% to 5% or 7% with increasing the feed amounts of OS particles from 10 to 500 or 700 mg, suggesting that the

sol-gel reactions in **Scheme 1** should proceed smoothly to provide the expected composites.

FE-SEM (Field Emission Scanning Electron Micrograph) photographs of the $R_F\text{-(VM-SiO}_{3/2})_n\text{-R}_F\text{/OS}$ composites (Run 5 in **Table 1**) have been recorded to clarify the formation of the composites, and the results are shown in **Figure 2**. FE-SEM picture of the pristine OS particles has been also illustrated in **Figure 2**, for comparison.

We can observe not only the uniformly coated-fluorinated oligomeric nanoparticles [$R_F\text{-(VM-SiO}_{3/2})_n\text{-R}_F$] on the OS particle surface but also the dispersed oligomeric nanoparticles near the OS particles (see **Figure 2(B)**). EDX (Energy Dispersive X-Ray) analyses measurements of the $R_F\text{-(VM-SiO}_{3/2})_n\text{-R}_F\text{/OS}$ composites (Run 5 in **Table 1**) also reveal that the atomic contents of silicon, fluorine and carbon are as follows (see **Table 2**).

The decrease of the contents of silicon from 44% to 14% in the composites, and the contents of fluorine (35%) and carbon (30%) indicate the presence of the fluorinated oligomer in the composites. The presence of Al in the original OS particles is due to the impurities in the particles. EDX mapping micrographs on the $R_F\text{-(VM-SiO}_{3/2})_n\text{-R}_F\text{/OS}$ composites (Run 5 in **Table 1**) and the pristine OS particles show that fluorine (blue-colored area) and carbon (red-colored area) related to the fluorinated oligomer are uniformly dispersed on the OS particle surface and around OS particles (see **Figure 3**).

We tried to study on the surface wettability of the $R_F\text{-(VM-SiO}_{3/2})_n\text{-R}_F\text{/OS}$

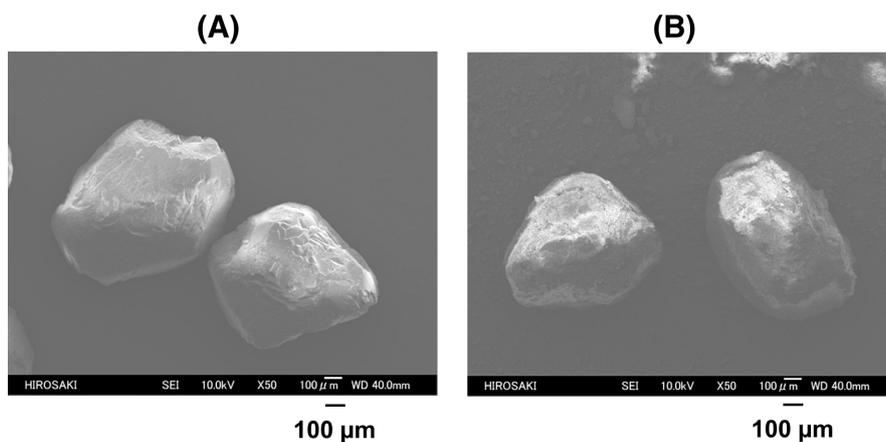


Figure 2. FE-SEM images of the $R_F\text{-(VM-SiO}_{3/2})_n\text{-R}_F\text{/OS}$ composites powders (Run 5 in **Table 1**) (B) and the pristine OS particles (A).

Table 2. The atomic contents of silicon, fluorine and carbon of the $R_F\text{-(VM-SiO}_{3/2})_n\text{-R}_F\text{/OS}$ composites (Run 5 in **Table 1**), and the pristine OS particles.

	Atomic contents (atm, %)			
	Si	F	C	Al
Pristine OS particles	44	0.0	0.0	1.0
$R_F\text{-(VM-SiO}_{3/2})_n\text{-R}_F\text{/OS}$ composites	14	35	30	0.0

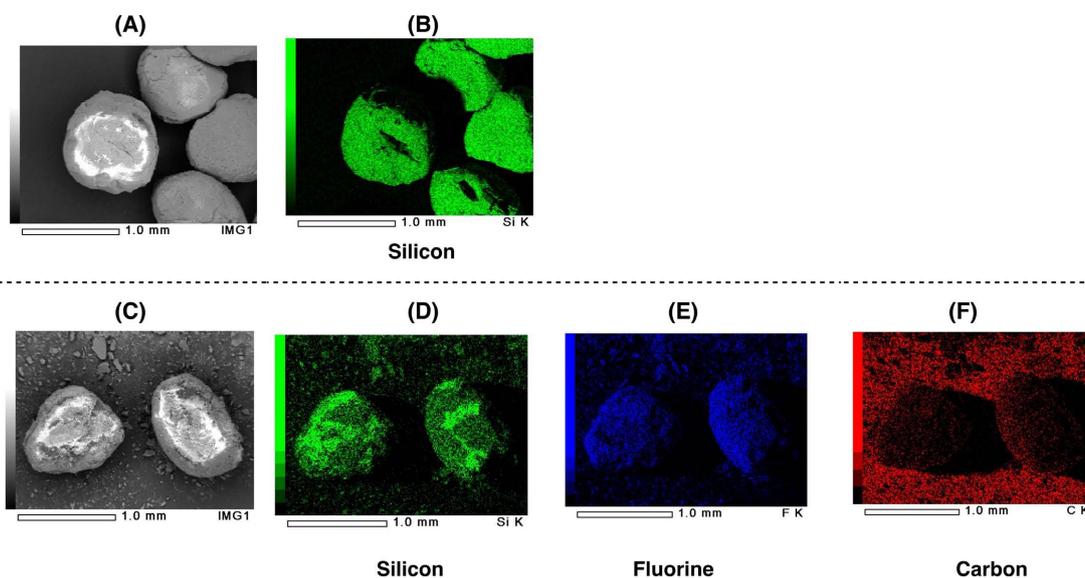


Figure 3. EDX (Energy Dispersive X-ray) mapping micrographs of silicon (B) of the pristine OS particles (A), and silicon (D), fluorine (E) and carbon (F) of the $R_F-(VM-SiO_{3/2})_n-R_F/OS$ composites powders (Run 5 in **Table 1**) (C).

composites powders: Runs 1-12 in **Table 1** and the pristine OS particles through the dodecane and water contact angle measurements. The results are revealed as followings:

	Contact angle value (Degree)	
	Dodecane	Water
Pristine OS particles	0	0
$R_F-(VM-SiO_{3/2})_n-R_F/OS$ composites (Runs 1 - 12)	0	180

Dodecane and water contact angle values of the pristine OS particles are 0 degree, respectively; however, each $R_F-(VM-SiO_{3/2})_n-R_F/OS$ composite powder (Runs 1 ~ 12 in **Table 1**) can exhibit a superoleophilic/superhydrophobic characteristic on its surface, because a dodecane droplet (2 μ L) can be easily adsorbed on the composite surface to exhibit the dodecane contact angle value: 0 degree, and water droplet (2 μ L) cannot be placed on the surface even after the pull-up process of the needlepoint from the surface during the water contact angle measurements owing to the superhydrophobic property in each case. We define the water contact angle value on its surface as 180 degrees in this case. In fact, as shown in **Figure 4(A)**, we can easily observe the sedimentation of the original OS particle powders into water; however, our present $R_F-(VM-SiO_{3/2})_n-R_F/OS$ composite powders can possess a perfect repellent ability toward water, floating on the water interface due to the superhydrophobicity related to the composite powders (see **Figure 4(B)**).

In this way, it was clarified that the present $R_F-(VM-SiO_{3/2})_n-R_F/OS$ composite powders can provide a superoleophilic/superhydrophobic property on their sur-

face. Thus, it is strongly expected that these composite powders should be applicable to the separation of the mixture of oil and water. Because, superoleophilic surface can provide a good affinity toward organic oils. Thus, superoleophilic/superhydrophobic surface should simultaneously repel water and adsorb oils effectively. We tried to apply the $R_F-(VM-SiO_{3/2})_n-R_F/OS$ composite powders (100 mg; Run 2 in **Table 1**) as the packing material for column chromatography to separate the mixture of water (3 mL) and 1,2-dichloroethane (3 mL), and the results are shown in **Figure 5**. We also tried to apply the $R_F-(VM-SiO_{3/2})_n-R_F/\mu-SiO_2$ powders, which were prepared under the similar conditions to those of **Scheme 1** and **Table 1** (see **Scheme 2**), as the packing material (100 mg) to separate the mixture of water and 1,2-dichloroethane. Because, the $R_F-(VM-SiO_{3/2})_n-R_F/\mu-SiO_2$ composites powders were found to exhibit the same surface wettability to that of the $R_F-(VM-SiO_{3/2})_n-R_F/OS$ composites powders. The results are also shown in **Figure 5(C)**, for comparison.

As shown in **Figure 5(B)**, we cannot separate the mixture of water and blue-colored 1,2-dichloroethane (DE) by using the pristine OS particles and $\mu-SiO_2$

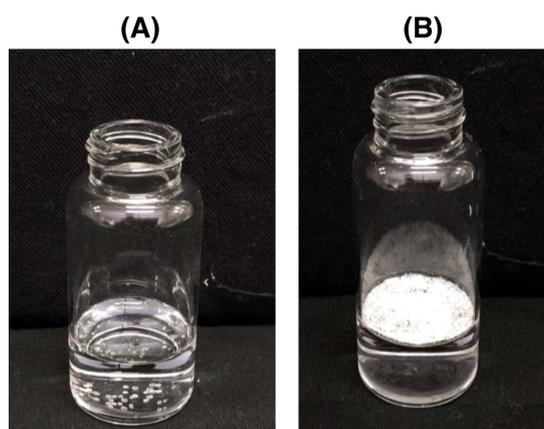
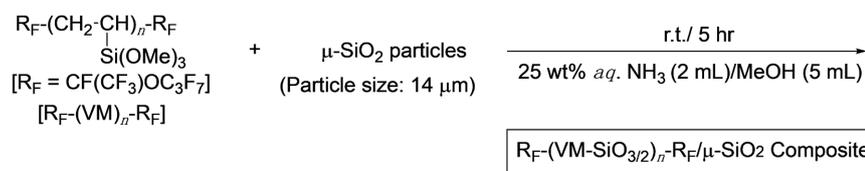


Figure 4. Photograph of the pristine OS powders in water: (A) and the $R_F-(VM-SiO_{3/2})_n-R_F/OS$ composite powders (Run 2 in **Table 1**) in water: (B).



	$R_F-(VM)_n-R_F$	$\mu-SiO_2$ particles	Yield (%) [*]	Size of the composites (μm) ^{**}	Content of oligomer in the composites (%) ^{***}
Run 1	50	10	73	8.1 ± 0.3	77
Run 2	50	50	67	9.5 ± 0.3	50

^{*}Yield was based on the used oligomer and $\mu-SiO_2$ particles

^{**}Determined by laser diffraction analysis measurements in methanol

^{***}Content of oligomer was estimated by the weight loss value at 800 °C of the composites by TGA measurements

Scheme 2. Preparation of $R_F-(VM-SiO_{3/2})_n-R_F/\mu-SiO_2$ composites.

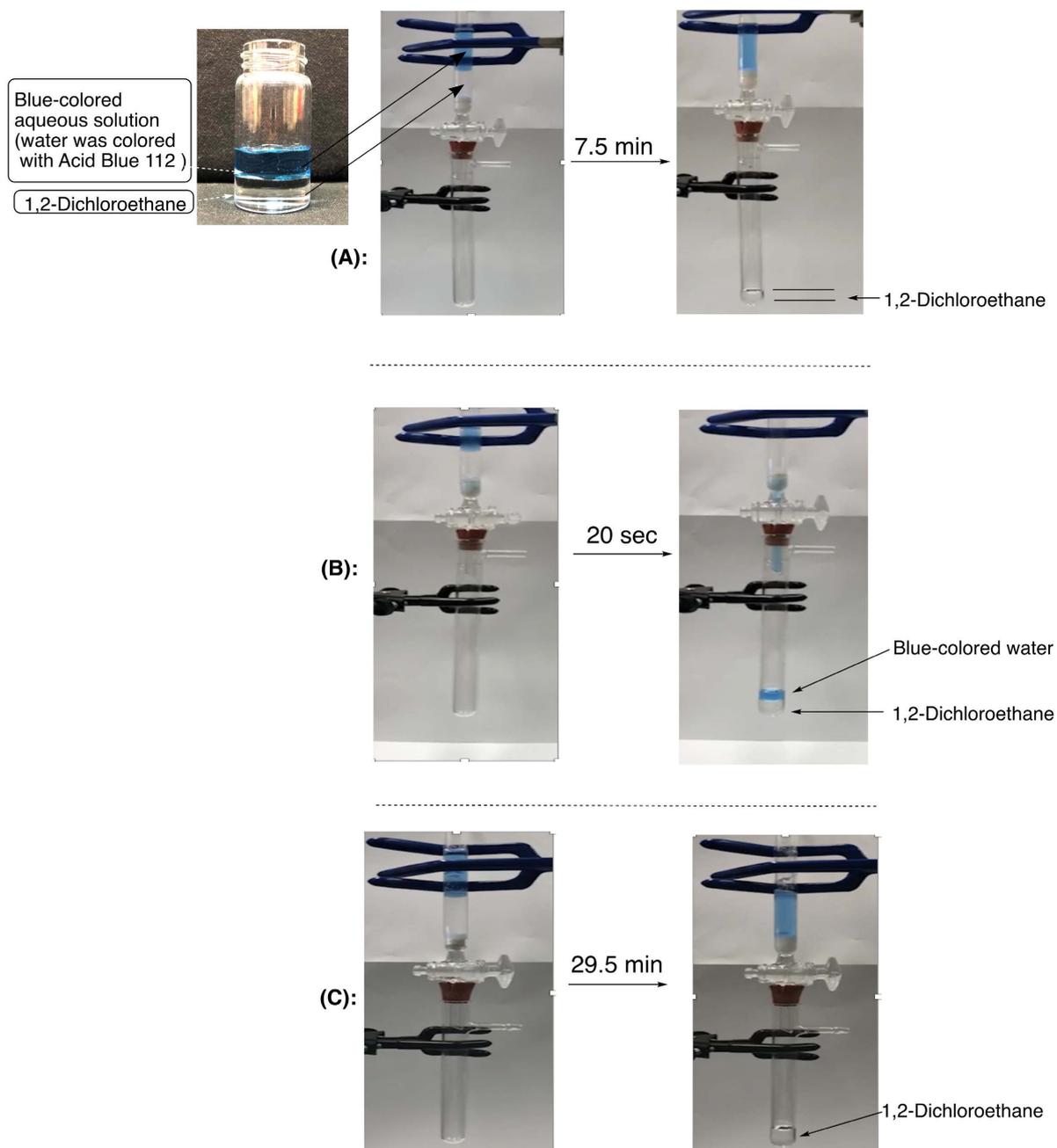


Figure 5. Separation of the mixture of blue-colored water and 1,2-dichloroethane by using the $R_F-(VM-SiO_{3/2})_n-R_F/OS$ composites powders (100 mg; Run 2 in **Table 1**): (A), pristine OS particles (100 mg): (B), and $R_F-(VM-SiO_{3/2})_n-R_F/\mu-SiO_2$ composites powders (100 mg; Run 2 in **Scheme 2**): (C) as the packing materials, respectively.

particles (data not shown), although the rapid filtration behavior (20 sec) was observed, as well as the use of the original $\mu-SiO_2$ particles (data not shown). On the other hand, we can smoothly isolate the colorless oil (DE) in 7.5 min by using the $R_F-(VM-SiO_{3/2})_n-R_F/OS$ composites powders (Run 2 in **Table 1**) as the packing material (see **Figure 5(A)**). In contrast, it was demonstrated that the $R_F-(VM-SiO_{3/2})_n-R_F/\mu-SiO_2$ composites powders (Run 2 in **Scheme 2**) requires the longer time from 7.5 to 29.5 min to isolate the transparent colorless DE un-

der similar conditions (see **Figure 5(C)**). This efficient and higher separation behavior in the $R_F-(VM-SiO_{3/2})_n-R_F/OS$ composites powders is due to the larger particle size ($\sim 840 \mu m$) of OS particles than that ($14 \mu m$) of the $\mu-SiO_2$ particles in the fluorinated oligomeric composites.

In addition to the separation of the mixture of water and DE, we tried to separate the W/O (oil: DE) emulsion by the use of the $R_F-(VM-SiO_{3/2})_n-R_F/OS$ composites powders (Run 2 in **Table 1**) as the packing material, and the results are shown in **Figure 6**.

As shown in **Figure 6**, we can isolate the transparent colorless oil (DE) by using the $R_F-(VM-SiO_{3/2})_n-R_F/OS$ composites powders (Run 2 in **Table 1**) as the packing material. Optical micrograph also revealed that the water droplet cannot be detected in the isolated oil at all, although water droplets can be easily observed in the original W/O emulsion as shown in **Table 3**. **Table 3** also shows that the colorless oils were quantitatively isolated in recovery rate from 81% - 85% even after the use of the O/W emulsions four times under similar conditions.

As mentioned above, particular attention has been devoted to the development of practical technology for removal of organic micropollutants, especially

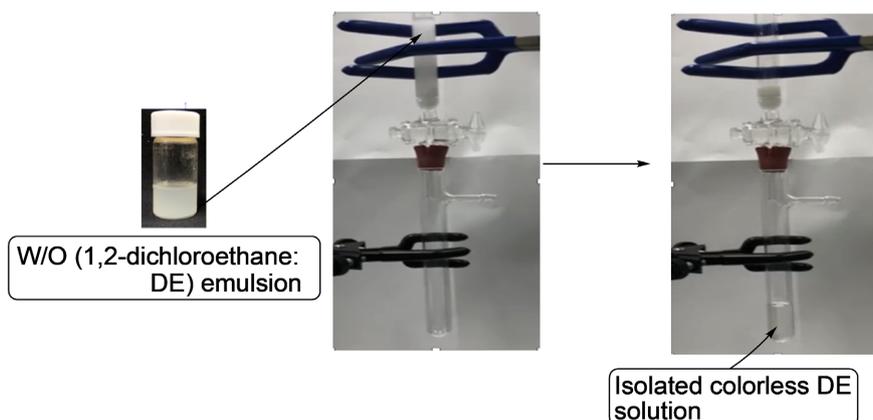


Figure 6. Separation of W/O (1,2-dichloroethane: DE) by using the $R_F-(VM-SiO_{3/2})_n-R_F/OS$ composites powders (100 mg: Run 2 in **Table 1**) as the packing material.

Table 3. Recovered rate and optical microscopy images of the separated oil from the W/O(oil: DE) emulsion by using the $R_F-(VM-SiO_{3/2})_n-R_F/OS$ composites powders (Run 2 in **Table 1**).

Cycle	1	2	3	4
Recovered rate (%)	83	82	85	81
Optical microscopy image				
Original W/O emulsion	1 cycle	2 cycle	3 cycle	4 cycle

fluorinated organic micropollutants from industrial wastewater [10]-[15]. Our present $R_F-(VM-SiO_{3/2})_n-R_F/OS$ composites are expected to enhance the removal ability toward the fluorinated organic compounds through the fluorophilic-fluorophilic interaction between the fluorinated moieties in organic molecules and the fluoroalkyl units in the composites. Superoleophilic/superhydrophobic property in the present fluorinated composites is also expected to enhance the removal ability of fluorinated compounds from aqueous solution through the effective oleophilic-oleophilic interaction between the organic molecules and the composites in aqueous solution with the superhydrophobicity on the composites. We herein tried to study on the removal ability of some fluorinated aromatic molecules including the corresponding non-fluorinated ones from aqueous methanol solutions by the use of the $R_F-(VM-SiO_{3/2})_n-R_F/OS$ composites powders (Run 1 in **Table 1**). The Schematic outline of the removal process is illustrated in **Figure 7**. We have also studied on the removal ability of the above indicated compounds from aqueous methanol solutions by using the $R_F-(VM-SiO_{3/2})_n-R_F/\mu-SiO_2$ composites powders (Run 1 in **Scheme 2**) under similar conditions, for comparison. The structures and concentrations (mg/dm^3) of the used fluorinated and non-fluorinated aromatic molecules are demonstrated in **Table 4**, and the removal ratios of these compounds are summarized in **Table 5**.

As shown in **Table 5**, the pristine OS particles and the $\mu-SiO_2$ particles exhibited the extremely poor removal ability for the fluorinated and non-fluorinated organic molecules; however, the $R_F-(VM-SiO_{3/2})_n-R_F/OS$ composites can give a higher removal ability toward the fluorinated organic molecules such as OFBP,

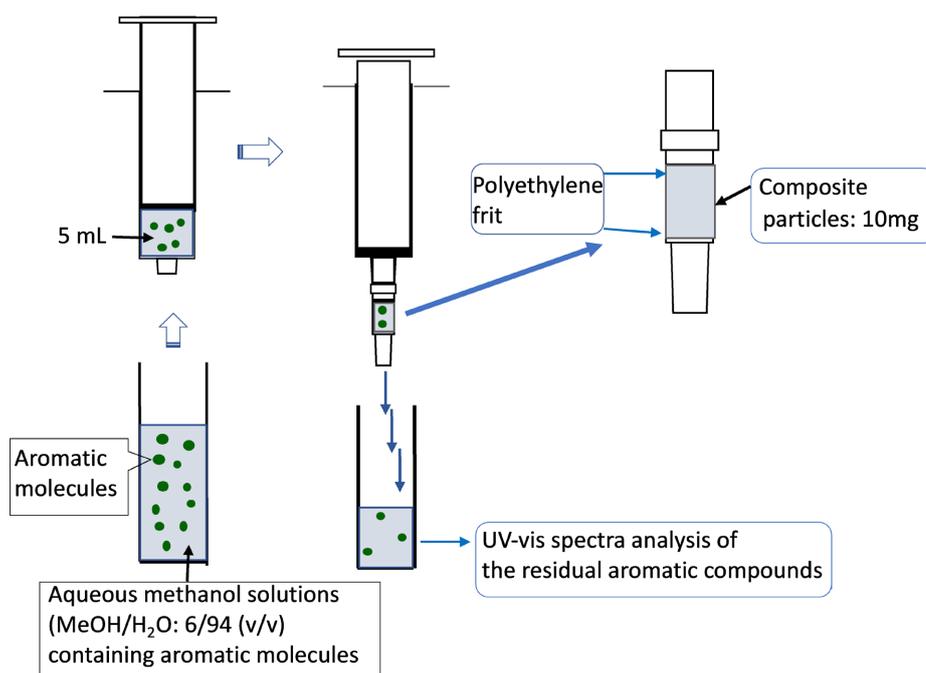


Figure 7. Schematic outline for the analysis of the removal ratio of aromatic molecules by using the $R_F-(VM-SiO_{3/2})_n-R_F/OS$ composites powders (10 mg; Run 1 in **Table 1**) and the $R_F-(VM-SiO_{3/2})_n-R_F/\mu-SiO_2$ composites powders (10 mg; Run 1 in **Scheme 2**).

Table 4. Structures and the concentrations of the used aromatic compounds for the analysis of the removal ratios.

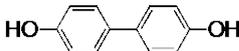
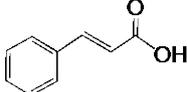
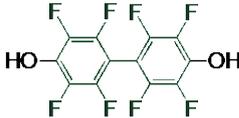
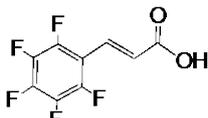
4,4'-Biphenol [BP-4,4']	Acetophenone [AP]	<i>trans</i> -Cinamic acid [CA]
		
20 mg/dm ³	10 mg/dm ³	30 mg/dm ³
Octafluorobiphenol [OFBP]	2',3',4',5',6'-Pentafluoroacetophenone [PFAP]	<i>trans</i> -2, 3, 4, 5, 6-Pentafluorocinamic acid [PFCA]
		
20 mg/dm ³	30 mg/dm ³	40 mg/dm ³

Table 5. Removal ratio (%) of aromatic compounds by using the R_F-(VM-SiO_{3/2})_n-R_F/OS composites powders (Run 1 in Table 1), pristine OS particles, the R_F-(VM-SiO_{3/2})_n-R_F/μ-SiO₂ composites powders (Run 1 in Scheme 2), and pristine μ-SiO₂ particles.

Composite	Removal ratio (%) of aromatic compounds					
	BP-4,4'	OFBP	AP	PFAP	CA	PFCA
R _F -(VM-SiO _{3/2}) _n -R _F /OS composites	0	26	46	86	1	19
OS particles	1	0	1	12	1	12
R _F -(VM-SiO _{3/2}) _n -R _F /μ-SiO ₂ composites	1	0	21	57	0	10
μ-SiO ₂ particles	0	0	3	11	0	0

PFAP and PFCA, compared to that of the corresponding non-fluorinated ones. Such higher removal ability toward the fluorinated molecules would be due to the effective fluorophilic-fluorophilic interaction between the fluorinated compounds and the fluorinated OS composites. In addition, it was verified that the R_F-(VM-SiO_{3/2})_n-R_F/OS composites can exhibit the superior removal ability of organic molecules to that of the R_F-(VM-SiO_{3/2})_n-R_F/μ-SiO₂ composites under similar conditions, indicating that the R_F-(VM-SiO_{3/2})_n-R_F/OS composites would have more preferable cavities to adsorb these organic molecules in aqueous methanol solutions than that of the corresponding fluorinated μ-SiO₂ composites.

4. Conclusion

We have applied fluoroalkyl end-capped vinyltrimethoxysilane oligomer [R_F-(VM)_n-R_F] to the facile preparation of the fluorinated oligomeric silica/sand composites [R_F-(VM-SiO_{3/2})_n-R_F/Ottawa sand (OS)] by the sol-gel reaction of the corresponding oligomer in the presence of micro-sized controlled OS particles

(particle size: 590 - 840 μm) under alkaline conditions. $\text{R}_F\text{-(VM-SiO}_{3/2})_n\text{-R}_F\text{/OS}$ composites powders thus obtained were found to exhibit a superoleophilic/superhydrophobic characteristic on the particle surface, applying to the efficient and smooth separation of not only the mixture of oil and water but also the W/O emulsion. In addition, the $\text{R}_F\text{-(VM-SiO}_{3/2})_n\text{-R}_F\text{/}\mu\text{-SiO}_2$ composites, which were prepared under similar sol-gel conditions by using the micro-sized silica gel particles (average particle size: 14 μm), afforded the similar surface wettability to apply the separation of the mixture of oil and water. It was clarified that we can observe the higher efficient and smooth separation ability for the separation of oil/water by the use of the fluorinated OS composites, compared to the fluorinated $\mu\text{-SiO}_2$ composites. Fluorinated OS composites were also found to exhibit a higher selective removal ability for the fluorinated organic molecules than that of the fluorinated $\mu\text{-SiO}_2$ composites. From such a point of view, our present fluorinated OS composites will have high potential for the practical application to not only the separation of oil and water but also the selective removal of fluorinated aromatic compounds from wastewater.

Funding

This work was partially supported by a Grant-in-Aid for Scientific Research 19K05027 from the Ministry of Education, Science, Sports, and Culture, Japan.

Conflicts of Interest

The authors declare no conflicts of interest regarding the publication of this paper.

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